



SHARRAH DUNLAP SAWYER, INC.

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# Panorama Planned Development

## Storm Drainage Feasibility Analysis

August 9, 2007

Romar Homes, Inc.

### Attachments:

- Soil conservation Service Map
- Shasta County Worksheets for Hydrology Analysis of Small Watersheds



### Panorama Planned Development- Storm Water Detention Feasibility Analysis

Purpose: Provide preliminary analysis of the major drainage basins that bisect the site and provide order of magnitude values for:

- Pre-development flow rates (25 yr & 100 yr)
- Post-development flow rates (25 yr & 100 yr)
- Volume of surface storage facilities for detention purposes (ac/ft)
- Define potential locations of detention facilities within the various drainage basins

#### Pre and Post Development Flows

Pre and post development flow where estimated utilizing Shasta County’s hydrology analysis for small water sheds (TR-55 & TR-20) for the basins defined on the projects storm drainage map (see attached).

The following pre and post development flow rates were estimated for the drainage basins defined on the drainage map:

Drainage Basin	Pre Development			Post Development		
	Area (acres)	25-year (cfs)	100-year (cfs)	Area (acres)	25-year (cfs)	100-year (cfs)
A	202	33	76	217	58	129
B	49	12	22	49	16	36
C	19	5	10	19	8	19
D	23	6	16	34	16	37

#### Storm Drainage Detention Volume

Storm drainage detention facilities storage volumes were estimated using TR-55 and TR-20 methods. The volumes for the various basins for a 100 year event are:

Basin	Volume (Acre Feet)
A	7.2
B	1.2
C	0.4
D	1.3

## Storm Drainage Map

Utilizing the projects preliminary grading plan and its definition of post development drainage patterns, the storm drainage plan was developed. This plan shows the following information:

### Drainage Basins Boundary Calculations:

Along the ridge tops where future grading will alter the basins boundary the adjusted boundary is shown. It should be noted that the western most drainage basin has been reduced in area from its original size by diverting post development drainage to Basin A where it shall be detained.

### Drainage Basin A:

Drainage Basin A was divided into two sub-basins (A-1 & A-2) to create two detention areas that could be located within the projects boundary. Preliminary analysis determined that due to the increased drainage area and the impervious nature of the diversions from the western basin the order of magnitude storage volume of Basin A is approximately 7.2 acre feet. The plan shows the location of these two detention areas (A-1 = 1.5 AF, A-2 = 6.0 AF).

In general the detention facilities will consist of a 10' wide embankment with 3:1 side slopes and a control structure meeting County requirements. Access to these facilities will be via public trails capable of supporting maintenance vehicles.

It should be noted that the existing stock pond at the upper reaches of Basin A was investigated as to its potential as a detention facility. Preliminary calculations indicated that due to the limited area upstream (26 acres) this existing pond could not be developed as a detention facility.

### Drainage Basins B, C, & D

These basins in the south easterly portion of the site are similar in nature due to the fact that the detention areas are all created by the future streets embankment and are contained within the open space between the up-slope lots. Access to the control facilities will be from the public street.

Basin B: The basin boundary is relatively unchanged from its pre-developed condition and its estimated storage volume is 1.5 acre feet.

Basin C: The basin boundary is only slightly increased from its pre-developed condition and its estimated storage volume is 0.6 acre feet.

Basin D: The basin area increases approximately 11 acres due to proposed development occurring in the north and east area adjacent to the basin. This basins estimated storage volume is 1.5 acre feet.

Subdivision Development South of ACID Channel

Pre and post development analysis of this portion of the project was not conducted. Due to the nature of the existing soils and its location with respect to other drainage facilities, if storm drainage detention is required it could easily be placed within the confines of the project.

Conclusion

As shown on the drainage plan, only a small portion of the open space areas with existing natural swales are utilized for storm water detention. If final drainage calculations indicate that more storm water detention facilities are required it can easily be accomplished.

Prepared by:

Frank E. Sawyer, P.E.  
RCE 24037



WESTERN DRAINAGE BASIN  
 • PRE DEVELOPED AREA = 33 AC  
 • POST DEVELOPED AREA = 23 AC  
 • DEVELOPEABLE AREA DIVERTED TO BASIN "A" = 10 AC  
 • NO DETENTION REQUIRED WITHIN BASIN



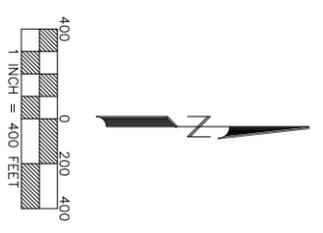
ADDITIONAL AREA OF POST DEVELOPMENT FLOW DIVERTED TO BASIN "A" 5 AC

ADDITIONAL AREA OF POST DEVELOPMENT FLOW DIVERTED TO BASIN "D" 11 AC

ACID DRAINAGE STRUCTURE UNDER CANAL  
 ACID CANAL  
 DIRECTION OF FLOW

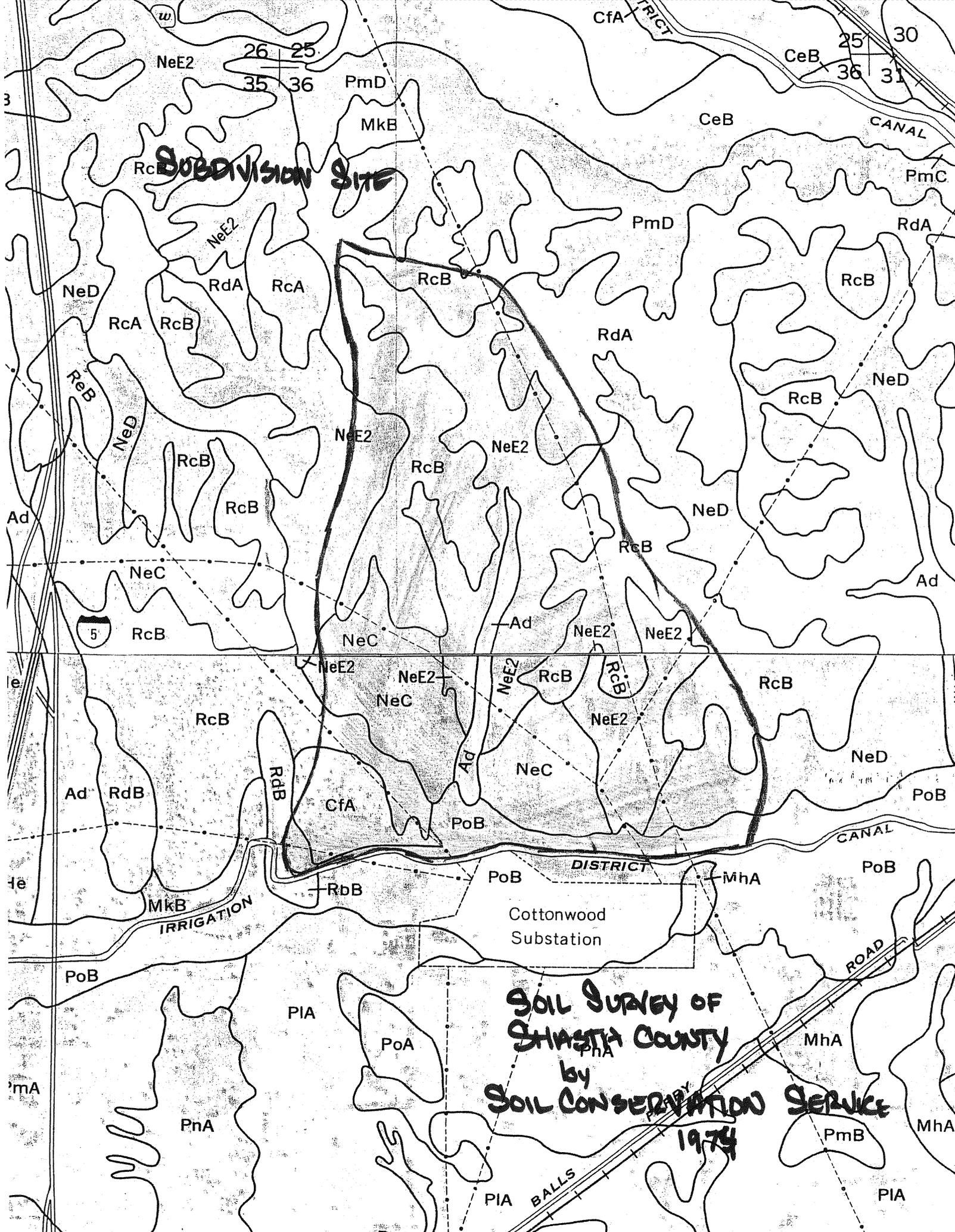
LEGEND

- A
- DRAINAGE BASIN DESIGNATION
- DETENTION AREA AND APPROXIMATE VOLUME (AC-FT)
- EARTH EMBANKMENT OR ROAD EMBANKMENT WITH FLOW CONTROL APPARATUS (MAX HEIGHT = 15 FT)
- PROPOSED INLET STRUCTURE AND UNDERGROUND STORM DRAINAGE PIPING
- APPROXIMATE POST CONSTRUCTION DRAINAGE BASIN BOUNDARY
- APPROXIMATE PRE CONSTRUCTION DRAINAGE BASIN BOUNDARY
- SURFACE DRAINAGE - NATURAL SWALE OR POST-DEVELOPMENT CONSTRUCTED



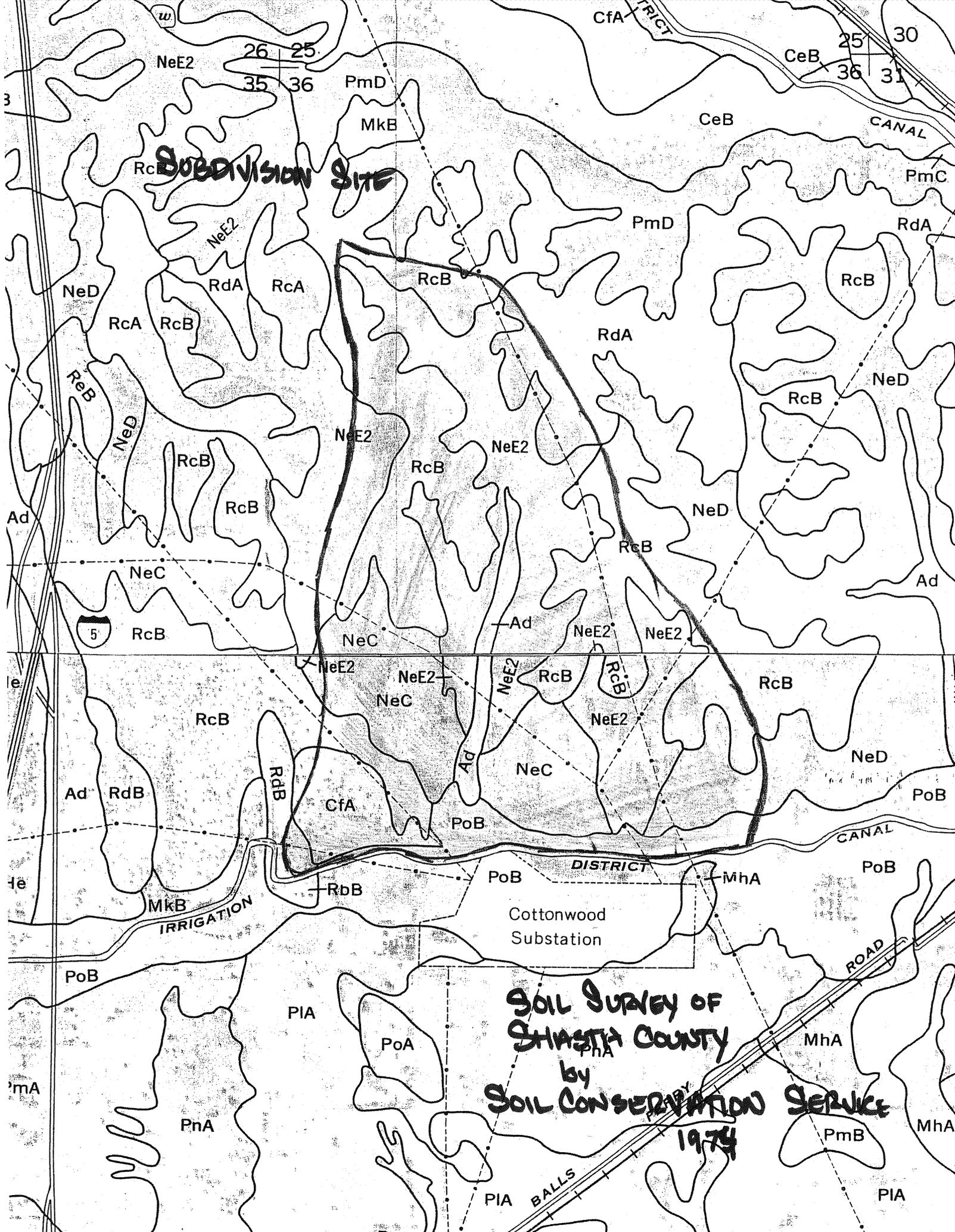
PANORAMA DEVELOPMENT  
 DRAINAGE MAP  
 FOR  
 STORM DRAINAGE DETENTION  
 FEASIBILITY ANALYSIS

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**SUBDIVISION SITE**

**SOIL SURVEY OF SHASTA COUNTY**  
by  
**SOIL CONSERVATION SERVICE**  
1974



**SUBDIVISION SITE**

**SOIL SURVEY OF SHASTA COUNTY**  
by  
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1974



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
Ad	B	Woodland	10	58	580
R <sub>2</sub> B, NeE <sub>2</sub> , NeC	C	Woodland	161.4	72	11620.8
R <sub>2</sub> A	D	Woodland	30.3	79	2393.7
TOTALS Σ A =			201.7	Σ A X CN =	14594.5

(b) 
$$\bar{CN} = \frac{\sum(A \times CN)}{\sum A} = \frac{14594.5}{201.7} = 72.4$$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME V<sub>24-D</sub>**

(a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2.0''}{P_{24-D}}$   $P_{6-D}$  =  $\frac{P_{6-D}}{P_{24-D}} = 0.513$

(b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $3.9''$   $P_{24-D}$

(c)  $R_{24-D}$  <sup>③</sup> = 1.4 in.

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times A \text{ ac.}$  =  $1.4 \times 12 = 23.5 \text{ ac-ft.}$

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>C</sub>**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$   1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$   2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$$CP = \frac{200 - 2}{CN} = \frac{200 - 2}{72.4} = 2.75$$

(c) FIND UNIT FLOW RATE (q) <sup>①</sup>

$$q = 77 \text{ csm/in}$$

(d)  $Q = q \times A_{mi^2} \times R_{24-D} = 32.3 \text{ CFS}$

$$Q = 32.3 \text{ CFS}$$

- ① See attachment no's 12 thru 14

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COUNTY OF SHASTA  
DEPARTMENT OF PUBLIC WORKS AND WATER AGENCY

HYDROLOGY ANALYSIS  
FOR  
SMALL WATERSHEDS

PROJECT NAME LOCUST ROAD SUBDIVISION SHEET 3 OF \_\_\_\_\_  
 DRAINAGE AREA NO. A SCALE Pre CALC. BY KIR DATE 12/06  
 SOURCE \_\_\_\_\_ CK'D. BY \_\_\_\_\_ DATE \_\_\_\_\_  
 (Attach Copy)

**STEP I - WATERSHED DATA**

(a) TOTAL DRAINAGE AREA (A)

A = 2017 ac.	=	A = 0.3 mi. <sup>2</sup>
L = 6700 ft.		L = 1.3 mi.

(b) LENGTH OF WATERSHED (L)

(c) ELEV. OF HIGHEST POINT IN WATERSHED (E<sub>h</sub>) = 620 ft.

(d) ELEV. OF LOWEST POINT IN WATERSHED (E<sub>1</sub>) = 460 ft.

(e) HEIGHT OF WATERSHED (H) = E<sub>h</sub> - E<sub>1</sub>

H = 160 ft.
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**STEP II - SELECT DESIGN FREQUENCY**

(a) CHECK APPROPRIATE BOXES

(b) BOXES CHECKED

USE

1.  A < 40 ac.

(1) only

10 year design

2.  40 ac. ≤ A ≤ 4 mi.<sup>2</sup>

(2) only  
or (1 and 4)  
or (1 and 5)

25 year design

3.  A > 4 mi.<sup>2</sup>

(3) or (6)  
or (2 and 5)

100 year design

4.  Streets with curb and gutter

5.  Roadway fills exceed 10 feet

6.  Sumps or retention ponds

**STEP III - FIND (T<sub>c</sub>)**

(a) FOR NATURAL DRAINAGE  
BASINS WHERE A > 4 mi.<sup>2</sup>

$$T_c = \frac{11.9L^3}{H_{ft}} \times 0.385 = \underline{\hspace{2cm}}$$

(b) ALL OTHER BASINS

$$T_c^{(2)} = \frac{K^{(1)}}{60} \frac{L^3}{H_{ft}} \times 0.20 = \underline{0.84}$$

K = 0.708

T <sub>c</sub> = 0.84 hrs.
----------------------------

① K = Land use constant (see attachment no. 1)  
 ② Use 5 minute minimum

AOF

**STEP IV - FIND WEIGHTED ( $\bar{CN}$ ) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
Ad	B	Woodland	10	58	580
RcB, NeE2, Nec	C	Woodland	1161.4	72	11620.8
KdA	D	Woodland	30.3	79	2393.7

TOTALS  $\Sigma A = 201.7$      $\Sigma A \times CN = 14594.5$

(b)  $\bar{CN} = \frac{\Sigma(A \times CN)}{\Sigma A} = \dots \dots \dots$      $\bar{CN} = 72.4$

- ① From "Soil Survey of Shasta County Area, Ca.," by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME  $V_{24-D}$**

(a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2.5}{P_{6-D}}$      $\frac{P_{6-D}}{P_{24-D}} = 0.101$

(b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $\frac{4.1}{P_{24-D}}$

(c)  $R_{24-D}$  <sup>③</sup>     $R_{24-D} = 1.5$  in.

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times A$  ac.     $V_{24-D} = 25.2$  ac-ft.

12

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @  $T_c$**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$CP = \frac{200}{CN} - 2 = \frac{200}{72.4} - 2$      $CP = 0.19$

(c) FIND UNIT FLOW RATE (q) <sup>①</sup>     $q = 169$  csm/in

(d)  $Q = q \times A_{mi^2} \times R_{24-D} = \dots$      $Q = 76$  CFS

① See attachment no's 12 thru 14

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COUNTY OF SHASTA  
DEPARTMENT OF PUBLIC WORKS AND WATER AGENCY

HYDROLOGY ANALYSIS  
FOR  
SMALL WATERSHEDS

PROJECT NAME LOCUST ROAD SUBDIVISION SHEET 5 OF \_\_\_\_\_  
 DRAINAGE AREA NO. A SCALE POST CALC. BY KR DATE 12/06  
 SOURCE \_\_\_\_\_ CK'D. BY \_\_\_\_\_ DATE \_\_\_\_\_  
 (Attach Copy)

**STEP I - WATERSHED DATA**

- |               |                                     |
|---------------|-------------------------------------|
| 217 AC        | 0.34                                |
| A = 201.7 ac. | A = <del>0.3</del> mi. <sup>2</sup> |
| L = 6320 ft.  | L = 1.2 mi.                         |
- (a) TOTAL DRAINAGE AREA (A)
- (b) LENGTH OF WATERSHED (L)
- (c) ELEV. OF HIGHEST POINT IN WATERSHED (E<sub>h</sub>) = 620 ft.
- (d) ELEV. OF LOWEST POINT IN WATERSHED (E<sub>l</sub>) = 460 ft.
- (e) HEIGHT OF WATERSHED (H) = E<sub>h</sub> - E<sub>l</sub> H = 160 ft.

**STEP II - SELECT DESIGN FREQUENCY**

- | (a) CHECK APPROPRIATE BOXES                                 | (b) BOXES CHECKED                        | USE  |
|---|--|--|
| 1. <input type="checkbox"/> A < 40 ac.                      | (1) only                                 | 10 year design <input type="checkbox"/>            |
| 2. <input type="checkbox"/> 40 ac. ≤ A ≤ 4 mi. <sup>2</sup> | (2) only<br>or (1 and 4)<br>or (1 and 5) | 25 year design <input checked="" type="checkbox"/> |
| 3. <input type="checkbox"/> A > 4 mi. <sup>2</sup>          | (3) or (6)<br>or (2 and 5)               | 100 year design <input type="checkbox"/>           |
| 4. <input type="checkbox"/> Streets with curb and gutter    |  |  |
| 5. <input type="checkbox"/> Roadway fills exceed 10 feet    |  |  |
| 6. <input type="checkbox"/> Sumps or retention ponds        |  |  |

**STEP III - FIND (T<sub>c</sub>)**

(a) FOR NATURAL DRAINAGE BASINS WHERE A > 4 mi.<sup>2</sup>

$$T_c = \frac{11.9L^3}{H_{ft}} = \frac{11.9 \times 6320^3}{160} = 0.385$$

(b) ALL OTHER BASINS

$$T_c^{(2)} = \frac{K^{(1)} L^3}{60 H_{ft}} = \frac{0.636 \times 6320^3}{60 \times 160} = 0.20$$

$$K = 0.50 \left( \frac{70}{201.7} \right) + 0.708 \left( \frac{131.7}{201.7} \right) = 0.636$$

T<sub>c</sub> = 0.13 hrs.

① K = Land use constant (see attachment no. 1)  
 ② Use 5 minute minimum

\* REVISION FOR ADDITIONAL FROM WESTERN BASIN = 10 AC & NORTH BOUNDARY SAC (TOTAL 15 AC)

58.8 AC

**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC <sup>②</sup> SOIL GROUP	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
Ad	B	Woodland	10	58	580
RcB, NeE2, NeC	C	Woodland	117.6	72	8467.2
RcB, NeE2, NeC	C	1/8 acre	43.8	90	3942
RdA	D	Woodland	4.1	79	323.9
RdA	D	1/4 acre	26.2	87	2279.4
* TOTALS Σ A =			2017	Σ A X CN =	155925
			217		

5292

16,942

(b)  $\frac{\sum(A \times CN)}{\sum A}$

$\bar{CN} = \frac{\sum(A \times CN)}{\sum A} = \dots$

$\bar{CN} = 77.78$  \*

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME V<sub>24-D</sub>**

(a)  $P_{6-D}$  (6 hour precipitation) ① =  $\frac{2''}{12} P_{6-D}$

$\frac{P_{6-D}}{P_{24-D}} = 0.513$  ✓

(b)  $P_{24-D}$  (24 hour precipitation) ② =  $\frac{3.9''}{12} P_{24-D}$

$R_{24-D} = 1.8$  in. ✓

(c)  $R_{24-D}$  ③

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times A$  ac. / 12

$V_{24-D} = 32.6$  ac-ft. \* ~~30.3~~

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>C</sub>**

(a) SELECT CURVE TYPE ①

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$CP = \frac{200 - 2}{P_{24-D}} = \frac{200 - 2}{3.9}$

CP = 0.15

(c) FIND UNIT FLOW RATE (q) ①

$t_c = 0.178$  hrs

q = 91.95 csm/in \*

(d)  $Q = q \times A_{mi^2} \times R_{24-D}$

Q = 49.1 CFS 58.1

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC <sup>②</sup> SOIL GROUP	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
SEE	25-YR CALCULATIONS				

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$  \_\_\_\_\_

$\bar{CN} = \frac{78*}{77}$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME (V<sub>24-D</sub>)**

(a) P<sub>6-D</sub> (6 hour precipitation) <sup>①</sup> =  $\frac{2.5}{P_{6-D}}$  P<sub>6-D</sub> =

$\frac{P_{6-D}}{P_{24-D}} = 0.61$

(b) P<sub>24-D</sub> (24 hour precipitation) <sup>②</sup> =  $\frac{4.1}{P_{24-D}}$  P<sub>24-D</sub>

(c) R<sub>24-D</sub> <sup>③</sup> . . . . .

R<sub>24-D</sub> = 1.9 in.

(d) V<sub>24-D</sub> (Total volume of runoff) = R<sub>24-D</sub> X ~~A~~ ac. <sup>217</sup>  
12

V<sub>24-D</sub> = ~~31.9~~ 34.3\* ac-ft.

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>C</sub>**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$   1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$   2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

CP =  $\frac{200}{CN} - 2 = \frac{200}{77} - 2$  . . . . .  
4.1

CP = 0.15 ✓

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

q = ~~194~~ 200 csm/in \*

(d) Q = q X A<sub>mi<sup>2</sup></sub> X R<sub>24-D</sub> = \_\_\_\_\_

Q = ~~110.6~~ CFS

- ① See attachment no's 12 thru 14

129 CFS \*



**STEP IV - FIND WEIGHTED ( $\bar{CN}$ ) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC <sup>②</sup> SOIL GROUP	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
RcB, NeE2, f88	C	Woodland	48.8	72	

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$  \_\_\_\_\_

$\bar{CN} = 72$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME  $V_{24-D}$**

(a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2}{P_{6-D}}$   $P_{6-D} =$  \_\_\_\_\_

$\frac{P_{6-D}}{P_{24-D}} = 0.513$

(b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $\frac{3.9}{P_{24-D}}$   $P_{24-D} =$  \_\_\_\_\_

(c)  $R_{24-D}$  <sup>③</sup> = \_\_\_\_\_

$R_{24-D} = 1.7$  in.

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times \frac{A \text{ ac.}}{12}$

$V_{24-D} = 6.9$  ac-ft.

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @  $T_c$**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$CP = \frac{200}{CN} - 2 = \frac{200}{72} - 2 =$  \_\_\_\_\_

CP = 0.2

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> = \_\_\_\_\_

q = 9.0 csm/in

(d)  $Q = q \times A_{mi^2} \times R_{24-D} =$  \_\_\_\_\_

Q = 12.2 CFS

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
SEE	25-yr	calculations			

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b)  $\frac{\sum (A \times CN)}{\sum A} =$  \_\_\_\_\_

**CN = 72**

- ① From "Soil Survey of Shasta County Area, Ca.," by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME (V<sub>24-D</sub>)**

(a) P<sub>6-D</sub> (6 hour precipitation) <sup>①</sup> = 2.5  $\frac{P_{6-D}}{P_{24-D}} =$  \_\_\_\_\_

**$\frac{P_{6-D}}{P_{24-D}} = 0.61$**

(b) P<sub>24-D</sub> (24 hour precipitation) <sup>②</sup> = 4.1 \_\_\_\_\_

(c) R<sub>24-D</sub> <sup>③</sup> \_\_\_\_\_

**R<sub>24-D</sub> = 1.15 in.**

(d) V<sub>24-D</sub> (Total volume of runoff) = R<sub>24-D</sub> X A ac.   
 12

**V<sub>24-D</sub> = 6.1 ac-ft.**

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>C</sub>**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$   1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$   2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

CP =  $\frac{200 - 2}{CN} =$  \_\_\_\_\_

**CP = 0.20**

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> \_\_\_\_\_

**q = 1.82 csm/in**

(d) Q = q X A<sub>mi</sub><sup>2</sup> X R<sub>24-D</sub> = \_\_\_\_\_

**Q = 21.8 CFS**

- ① See attachment no's 12 thru 14

COUNTY OF SHASTA  
DEPARTMENT OF PUBLIC WORKS AND WATER AGENCY

HYDROLOGY ANALYSIS  
FOR  
SMALL WATERSHEDS

PROJECT NAME LOWUST RD SUBDIVISION SHEET 13 OF \_\_\_\_\_  
DRAINAGE AREA NO. B SCALE POST CALC. BY KR DATE 12/06  
SOURCE \_\_\_\_\_ CK'D. BY \_\_\_\_\_ DATE \_\_\_\_\_  
(Attach Copy)

STEP I - WATERSHED DATA

- (a) TOTAL DRAINAGE AREA (A) A = 48.8 ac. = A = 0.08 mi.<sup>2</sup>
- (b) LENGTH OF WATERSHED (L) L = 2272 ft. L = 0.4 mi.
- (c) ELEV. OF HIGHEST POINT IN WATERSHED (E<sub>h</sub>) = 580 ft.
- (d) ELEV. OF LOWEST POINT IN WATERSHED (E<sub>l</sub>) = 400 ft.
- (e) HEIGHT OF WATERSHED (H) = E<sub>h</sub> - E<sub>l</sub> H = 170 ft.

STEP II - SELECT DESIGN FREQUENCY

- | (a) CHECK APPROPRIATE BOXES                                 | (b) BOXES CHECKED                        | USE  |
|---|--|--|
| 1. <input type="checkbox"/> A < 40 ac.                      | (1) only                                 | 10 year design <input type="checkbox"/>            |
| 2. <input type="checkbox"/> 40 ac. ≤ A ≤ 4 mi. <sup>2</sup> | (2) only<br>or (1 and 4)<br>or (1 and 5) | 25 year design <input checked="" type="checkbox"/> |
| 3. <input type="checkbox"/> A > 4 mi. <sup>2</sup>          | (3) or (6)<br>or (2 and 5)               | 100 year design <input type="checkbox"/>           |
| 4. <input type="checkbox"/> Streets with curb and gutter    |  |  |
| 5. <input type="checkbox"/> Roadway fills exceed 10 feet    |  |  |
| 6. <input type="checkbox"/> Sumps or retention ponds        |  |  |

STEP III - FIND (T<sub>c</sub>)

(a) FOR NATURAL DRAINAGE BASINS WHERE A > 4 mi.<sup>2</sup>       $T_c = \frac{11.9L^3}{H_{ft}} \times 0.385 = \underline{\hspace{2cm}}$

(b) ALL OTHER BASINS       $T_c^{(2)} = \frac{K^{(1)}}{60} \frac{L^3}{H_{ft}} \times 0.20 = \underline{\hspace{2cm}}$

K = 0.636

T<sub>c</sub> = 0.42 hrs.

① K = Land use constant (see attachment no. 1)  
② Use 5 minute minimum

\* NO CHANGE THIS BASIN

**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
RcB, NeEz, PoB	C	WOODLAND	38.5	72	2772
RcB, NeEz, PoB	C	1/8 acre	10.3	90	927
TOTALS Σ A =			48.8	Σ A X CN =	3699

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} = \dots$

**̄CN = 75.8**

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME V<sub>24-D</sub>**

(a) P<sub>6-D</sub> (6 hour precipitation) <sup>①</sup> =  $\frac{2}{P_{24-D}}$  P<sub>6-D</sub> =

**$\frac{P_{6-D}}{P_{24-D}} = 0.513$**

(b) P<sub>24-D</sub> (24 hour precipitation) <sup>②</sup> =  $\frac{3.9}{P_{24-D}}$  P<sub>24-D</sub>

(c) R<sub>24-D</sub> <sup>③</sup> . . . . .

**R<sub>24-D</sub> = 1.7 in.**

(d) V<sub>24-D</sub> (Total volume of runoff) = R<sub>24-D</sub> X A ac. / 12

**V<sub>24-D</sub> = 0.9 ac-ft.**

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>C</sub>**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

CP =  $\frac{200}{\bar{CN}} - 2 = \frac{200}{75.8} - 2 = \dots$

**CP = 0.16**

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

**q = 114 csm/in**

(d) Q = q X A<sub>mi<sup>2</sup></sub> X R<sub>24-D</sub> = . . . . .

**Q = 15.5 CFS**

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
See	25-year calculations				

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b) 
$$\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$$

$\bar{CN} = 75.8$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and P. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME  $V_{24-D}$**

(a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2.5}{P_{6-D}}$   $P_{6-D} =$

$\frac{P_{6-D}}{P_{24-D}} = 0.61$

(b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $\frac{4.1}{P_{24-D}}$   $P_{24-D} =$

$R_{24-D} = 1.8$  in.

(c)  $R_{24-D}$  <sup>③</sup> . . . . .

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times A$  ac.   
 12

$V_{24-D} = 7.3$  ac-ft.

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @  $T_c$**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$$CP = \frac{200 - 2}{CN} =$$

CP = 0.16

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

q = 253 csm/in

(d)  $Q = q \times A_{mi^2} \times R_{24-D} =$  \_\_\_\_\_

Q = 36.4 CFS

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC <sup>②</sup> SOIL GROUP	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
ReB, NEEZ, NEC, PdB	C	Woodland	19.4	72	
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$  \_\_\_\_\_

**̄CN = 72**

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME V<sub>24-D</sub>**

(a) P<sub>6-D</sub> (6 hour precipitation) <sup>①</sup> =  $\frac{2}{12} P_{6-D} =$  \_\_\_\_\_

**$\frac{P_{6-D}}{P_{24-D}} = 0.513$**

(b) P<sub>24-D</sub> (24 hour precipitation) <sup>②</sup> =  $\frac{3.9}{12} P_{24-D} =$  \_\_\_\_\_

**R<sub>24-D</sub> = 1.7 in.**

(c) R<sub>24-D</sub> <sup>③</sup> . . . . .

(d) V<sub>24-D</sub> (Total volume of runoff) = R<sub>24-D</sub> X A ac. / 12

**V<sub>24-D</sub> = 2.7 ac-ft.**

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>c</sub>**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

CP =  $\frac{200 - 2}{CN} =$  \_\_\_\_\_

**CP = 0.20**

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

**q = 100 csm/in**

(d) Q = q X A<sub>mi<sup>2</sup></sub> X R<sub>24-D</sub> = \_\_\_\_\_

**Q = 5.1 CFS**

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC <sup>②</sup> SOIL GROUP	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
See 25-yr Calculations					

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b) 
$$\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$$

$\bar{CN} = 72$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME V<sub>24-D</sub>**

(a) P<sub>6-D</sub> (6 hour precipitation) ① =  $\frac{2.5}{12} P_{6-D} =$

$\frac{P_{6-D}}{P_{24-D}} = 0.61$

(b) P<sub>24-D</sub> (24 hour precipitation) ② =  $\frac{4.1}{12} P_{24-D}$

$R_{24-D} = 1.5 \text{ in.}$

(c) R<sub>24-D</sub> ③

(d) V<sub>24-D</sub> (Total volume of runoff) = R<sub>24-D</sub> X  $\frac{A \text{ ac.}}{12}$

$V_{24-D} = 2.4 \text{ ac-ft.}$

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>c</sub>**

(a) SELECT CURVE TYPE ①

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$$CP = \frac{200}{CN} - 2 =$$

$CP = 0.20$

(c) FIND UNIT FLOW RATE (q) ①

$q = 235 \text{ csm/in}$

(d) Q = q X A<sub>mi<sup>2</sup></sub> X R<sub>24-D</sub> =

$Q = 10.6 \text{ CFS}$

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
	C	Woodland	5.1	72	367.2
	C	1/4 acre	14.3	83	1186.9
TOTALS $\Sigma A =$			19.4		$\Sigma A \times CN = 1554.1$

(b)  $\bar{CN} = \frac{\Sigma(A \times CN)}{\Sigma A} = \frac{1554.1}{19.4} = 80.1$

- ① From "Soil Survey of Shasta County Area, Ca.," by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME  $V_{24-D}$**

- (a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2}{P_{6-D}}$   $\frac{P_{6-D}}{P_{24-D}} =$   $\frac{P_{6-D}}{P_{24-D}} = 0.513$
- (b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $\frac{3.9}{P_{24-D}}$   $R_{24-D} = 2.0$  in.
- (c)  $R_{24-D}$  <sup>③</sup>  $V_{24-D} = 3.2$  ac-ft.
- (d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times A$  ac.  $V_{24-D} = 3.2$  ac-ft.
- ① See attachment no's 4 thru 6
  - ② See attachment no's 7 thru 9
  - ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @  $T_c$**

- (a) SELECT CURVE TYPE <sup>①</sup>
- 1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$
- (b) CALCULATE CURVE PARAMETER (CP)
- $CP = \frac{200 - 2}{\frac{CN}{P_{24-D}}} = \frac{200 - 2}{\frac{80.1}{3.9}}$   $CP = 0.13$
- (c) FIND UNIT FLOW RATE (q) <sup>①</sup>  $q = 129$  csm/in
- (d)  $Q = q \times A_{mi^2} \times R_{24-D} =$   $Q = 7.7$  CFS
- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
See 25-yr Calculations					

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b) 
$$\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$$

$\bar{CN} = 80.1$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME V<sub>24-D</sub>**

(a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2.5}{P_{6-D}}$   $P_{6-D} =$

$\frac{P_{6-D}}{P_{24-D}} = 0.61$

(b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $\frac{4.1}{P_{24-D}}$   $P_{24-D}$

(c)  $R_{24-D}$  <sup>③</sup> . . . . .

$R_{24-D} = 2.2$  in.

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times A$  ac.   
 12

$V_{24-D} = 3.6$  ac-ft.

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>c</sub>**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$   1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$   2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$CP = \frac{200 - 2}{CN} = \frac{200 - 2}{80.1} =$  \_\_\_\_\_

CP = 0.13

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

q = 283 csm/in

(d)  $Q = q \times A_{mi^2} \times R_{24-D} =$  \_\_\_\_\_

Q = 18.7 CFS

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED ( $\bar{CN}$ ) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
	C	Woodland	22.6	72	

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$  \_\_\_\_\_

$\bar{CN} = 72$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME  $V_{24-D}$**

(a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2}{12} P_{6-D} =$  \_\_\_\_\_

$\frac{P_{6-D}}{P_{24-D}} = 0.513$

(b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $\frac{3.9}{12} P_{24-D} =$  \_\_\_\_\_

$R_{24-D} = 1.5$  in.

(c)  $R_{24-D}$  <sup>③</sup> . . . . .

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times \frac{A \text{ ac.}}{12}$

$V_{24-D} = 2.8$  ac-ft.

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @  $T_C$**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$CP = \frac{200}{CN} - 2 =$  \_\_\_\_\_

CP = 0.20

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

q = 100 csm/in

(d)  $Q = q \times A_{mi^2} \times R_{24-D} =$  \_\_\_\_\_

Q = 6.0 CFS

- ① See attachment no's 12 thru 14



**STEP IV - FIND WEIGHTED ( $\bar{CN}$ ) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
TOTALS $\sum A =$			_____	$\sum A \times CN =$	_____

See 25-yr Calculations

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$  \_\_\_\_\_

$\bar{CN} = 72$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME  $V_{24-D}$**

(a)  $P_{6-D}$  (6 hour precipitation) <sup>①</sup> =  $\frac{2.5}{4.1} P_{6-D} =$  \_\_\_\_\_

(b)  $P_{24-D}$  (24 hour precipitation) <sup>②</sup> =  $\frac{4.1}{24-D} P_{24-D} =$  \_\_\_\_\_

$\frac{P_{6-D}}{P_{24-D}} = 0.61$

(c)  $R_{24-D}$  <sup>③</sup> . . . . .

$R_{24-D} = 1.7$  in.

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times A$  ac.   
 12

$V_{24-D} = 3.2$  ac-ft.

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

**STEP VI - FIND PEAK FLOW RATE (Q) @  $T_C$**

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$   1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$   2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$CP = \frac{200 - 2}{CN} = \frac{200 - 2}{72} =$  \_\_\_\_\_

CP = 0.2

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

q = 235 csm/in

(d)  $Q = q \times A_{mi^2} \times R_{24-D} =$  \_\_\_\_\_

Q = 16.0 CFS

- ① See attachment no's 12 thru 14



STEP IV - FIND WEIGHTED (CN) CURVE NUMBER

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup>	CN <sup>⑤</sup>	AREA X CN
	C	1/4 acre	<del>22.6</del> 33.6*	83	

TOTALS  $\sum A =$  \_\_\_\_\_  $\sum A \times CN =$  \_\_\_\_\_

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$  \_\_\_\_\_

$\bar{CN} = 83$  ✓

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

STEP V - FIND RUNOFF VOLUME V<sub>24-D</sub>

(a) P<sub>6-D</sub> (6 hour precipitation) <sup>①</sup> =  $\frac{2}{3.9} P_{6-D} =$  \_\_\_\_\_

$\frac{P_{6-D}}{P_{24-D}} = 0.513$  ✓

(b) P<sub>24-D</sub> (24 hour precipitation) <sup>②</sup> =  $\frac{3.9}{12} P_{24-D}$

R<sub>24-D</sub> = 2.3 in. ✓

(c) R<sub>24-D</sub> <sup>③</sup> . . . . .

(d) V<sub>24-D</sub> (Total volume of runoff) = R<sub>24-D</sub> X A ac.   
 12

V<sub>24-D</sub> = ~~4.2~~ 6.44 ac-ft. \*

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

STEP VI - FIND PEAK FLOW RATE (Q) @ T<sub>c</sub>

(a) SELECT CURVE TYPE <sup>①</sup>

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$      1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$      2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

CP =  $\frac{200 - 2}{CN} = \frac{200 - 2}{83} = \frac{198}{83} = 2.38$

CP = 0.11 ✓

(c) FIND UNIT FLOW RATE (q) <sup>①</sup> . . . . .

q = 130 csm/in ✓

(d) Q = q X A<sub>mi</sub><sup>2</sup> X R<sub>24-D</sub> = \_\_\_\_\_

Q = ~~12.0~~ CFS

- ① See attachment no's 12 thru 14

\* 15.80 CFS



**STEP IV - FIND WEIGHTED (CN) CURVE NUMBER**

(a) SOIL SYMBOL <sup>①</sup>	HYDROLOGIC SOIL GROUP <sup>②</sup>	LAND USE <sup>③</sup>	AREA <sup>④</sup> ac.	CN <sup>⑤</sup>	AREA X CN
TOTALS $\sum A =$				$\sum A \times CN =$	

*See 25-yr Calculations*

(b)  $\bar{CN} = \frac{\sum(A \times CN)}{\sum A} =$  \_\_\_\_\_

$\bar{CN} = 83$

- ① From "Soil Survey of Shasta County Area, Ca., "by the U.S. Dept. of Agriculture, S. C. S. and F. S., Aug. 1974.
- ② See attachment no. 2
- ③ See attachment no. 3
- ④ Include copy of soil survey map with soil boundaries delineated or other appropriate documentation.

**STEP V - FIND RUNOFF VOLUME  $V_{24-D}$**

(a)  $P_{6-D}$  (6 hour precipitation) ① =  $\frac{2.5}{P_{6-D}}$   $P_{6-D} =$  \_\_\_\_\_

$\frac{P_{6-D}}{P_{24-D}} = 0.61$

(b)  $P_{24-D}$  (24 hour precipitation) ② =  $\frac{4.1}{P_{24-D}}$   $P_{24-D} =$  \_\_\_\_\_

(c)  $R_{24-D}$  ③ .....  $R_{24-D} =$  \_\_\_\_\_

$R_{24-D} = 2.4$  in.

(d)  $V_{24-D}$  (Total volume of runoff) =  $R_{24-D} \times \frac{336}{12}$  ac.  $V_{24-D} =$  \_\_\_\_\_

$V_{24-D} = 45$  ac-ft.

- ① See attachment no's 4 thru 6
- ② See attachment no's 7 thru 9
- ③ See attachment no's 10 and 11

\* 6.7 AC-FT

**STEP VI - FIND PEAK FLOW RATE (Q) @  $T_c$**

(a) SELECT CURVE TYPE ①

1A  $\frac{P_{6-D}}{P_{24-D}} < 0.518$   1  $0.518 \leq \frac{P_{6-D}}{P_{24-D}} \leq 0.639$   2  $0.639 < \frac{P_{6-D}}{P_{24-D}} \leq 0.767$

(b) CALCULATE CURVE PARAMETER (CP)

$CP = \frac{200}{CN} - 2 = \frac{200}{83} - 2 =$  \_\_\_\_\_

$CP = 0.10$

(c) FIND UNIT FLOW RATE (q) ① .....  $q =$  \_\_\_\_\_

$q = 288$  \*  $290$  csm/in

(d)  $Q = q \times A_{mi^2} \times R_{24-D} =$  \_\_\_\_\_ CFS

$Q = 276$  CFS

- ① See attachment no's 12 thru 14

\* 36.80 CFS



# SHARRAH DUNLAP SAWYER, INC.

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PAGE \_\_\_\_\_ OF \_\_\_\_\_  
JOB NO: 06.0198.000  
CALC: KZ CHKD: \_\_\_\_\_ DATE: 12/06  
JOB NAME: Locust Rd  
Subdivision

Determine Preliminary Detention required for Basins A, B, C, & D

$$V_{req'd} = (Q_{in} - Q_{out})(3)(T_{c_{post}})(0.5)(60)(K) \quad K = 1.5$$

Basin A:  $V_{25} = (49.1 - 32.3)(3)(43.8)(0.5)(60)(1.5) = 99338 \text{ CF} = 2.3 \text{ ac-ft}$

\*  $V_{100} = (110.6 - 76)(3)(43.8)(0.5)(60)(1.5) = 204590 \text{ CF} = \underline{\underline{4.7 \text{ ac-ft}}}$

Basin B:  $V_{25} = (15.5 - 12.2)(3)(25.2)(0.5)(60)(1.5) = 11227 \text{ CF} = 0.3 \text{ ac-ft}$

$V_{100} = (36.4 - 21.8)(3)(25.2)(0.5)(60)(1.5) = 49469 \text{ CF} = \underline{\underline{1.2 \text{ ac-ft}}}$

Basin C:  $V_{25} = (7.7 - 5.1)(3)(16.8)(0.5)(60)(1.5) = 5897 \text{ CF} = 0.2 \text{ ac-ft}$

$V_{100} = (18.7 - 10.6)(3)(16.8)(0.5)(60)(1.5) = 18371 \text{ CF} = \underline{\underline{0.4 \text{ ac-ft}}}$

Basin D:  $V_{25} = (12 - 6)(3)(19.8)(0.5)(60)(1.5) = 16038 \text{ CF} = 0.4 \text{ ac-ft}$

\*  $V_{100} = (27.6 - 16)(3)(19.8)(0.5)(60)(1.5) = 31007 \text{ CF} = \underline{\underline{0.7 \text{ ac-ft}}}$

Tributary area to (e) pond =  $\frac{1400 \times 800}{43560} = 25.7 \text{ acres}$

$\frac{25.7}{201.7} = 12.7\% \quad \text{not enough area}$

\* REVISIONS DUE TO POST DEVELOPMENT DRAINAGE BASIN INCREASES

BASIN "A"

$V_{100} = (129 - 76)(3)(43.8)(0.5)(60)(1.5) = 313,389 = 7.2 \text{ AC-FT}$

BASIN "D"

$V_{100} = (36.8 - 16)(3)(19.8)(0.5)(60)(1.5) = 55,600 \text{ SF} = 1.3 \text{ AC FT}$